TILITY PATENT APPLICATION TRANSMITTAL (Large Entity)

Docket No. 1559A1

(Only for new nonprovisional applications under 37 CFR 1.53(b))

Total Pages in this Submission 38

TO THE ASSISTANT COMMISSIONER FOR PATENTS

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Enclos			lication claims th	ne benefits	s of U.S. Provisional Application No. 60/167,386.
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1.	×	Filin	g fee as calculated and	transmitted a	as described below
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2.	×	Spe	cification having		pages and including the following:
	a.	×	Descriptive Title of the	Invention	
	b.	\boxtimes	Cross References to R	telated Applic	cations (if applicable)
	C.		Statement Regarding F	ederally-spo	onsored Research/Development (if applicable)
	d.		Reference to Microfich	e Appendix (if applicable)
	e.	X	Background of the Inve	ention	
	f.	×	Brief Summary of the I	nvention	
	g.	×	Brief Description of the	Drawings (if	f drawings filed)
	h.	×	Detailed Description		
	i.	\boxtimes	Claim(s) as Classified	Below	
	j.	X	Abstract of the Disclos	ure	

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Application Elements (Continued) ☑ Drawing(s) (when necessary as prescribed by 35 USC 113) Number of Sheets Formal Number of Sheets 1 X Informal Oath or Declaration Newly executed (original or copy) Unexecuted J Copy from a prior application (37 CFR 1.63(d)) (for continuation/divisional application only) b. 🔲 ☐ Without Power of Attorney With Power of Attorney c. 🔀 d. DELETION OF INVENTOR(S) Signed statement attached deleting inventor(s) named in the prior application, O see 37 C.F.R. 1.63(d)(2) and 1.33(b). ji [≅] 5. ☐ Incorporation By Reference (usable if Box 4b is checked) The entire disclosure of the prior application, from which a copy of the oath or declaration is supplied under Box 4b, is considered as being part of the disclosure of the accompanying application and is hereby H 1 incorporated by reference therein. 6. ☐ Computer Program in Microfiche (Appendix) ☐ Nucleotide and/or Amino Acid Sequence Submission (if applicable, all must be included) a. Paper Copy b. Computer Readable Copy (identical to computer copy) c. Statement Verifying Identical Paper and Computer Readable Copy **Accompanying Application Parts** ☐ Assignment Papers (cover sheet & document(s)) ☐ 37 CFR 3.73(B) Statement (when there is an assignee) ☐ English Translation Document (if applicable) Copies of IDS Citations ☐ Information Disclosure Statement/PTO-1449 Preliminary Amendment 13. Acknowledgment postcard 14. Certificate of Mailing

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		Accompanying Application Parts (Continued)	
15.		Certified Copy of Priority Document(s) (if foreign priority is claimed)	
16.		Additional Enclosures (please identify below):	
14 14		Request That Application Not Be Published Pursuant To 35 U.S.C. 122(b)(2) Pursuant to 35 U.S.C. 122(b)(2), Applicant hereby requests that this patent application not be	
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Fee Calculation and Transmittal

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For	#Filed	#Allowed	#Extra		Rate	Fee
otal Claims	38	- 20 =	18	×	\$18.00	\$324.00
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OTHER FEE (spe	cify purpose)					\$0.00
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Signature

Dated: November 16, 2000

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Pittsburgh, Pennsylvania

CC.

LOW SHADING COEFFICIENT AND LOW EMISSIVITY COATINGS AND COATED ARTICLES

CROSS-REFERENCE TO RELATED APPLICATION

This application claims the benefits of United States Provisional Application No. 60/167,386, filed November 24, 1999, entitled "LOW SHADING COEFFICIENT AND LOW EMISSIVITY COATINGS AND COATED ARTICLES", which is herein incorporated by reference.

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FIELD OF THE INVENTION

This invention relates generally to heat-reflective and solar-control glazing materials such as multilayered coatings and to articles, e.g. windows or insulating glass 15 units, incorporating such coatings and, more particularly, to solar-control metal oxide-containing coatings which may form solar-control articles having intermediate levels of luminous (visible light) transmittance, relatively low shading coefficient and emissivity, and acceptable levels of luminous (visible light) reflectance.

DISCUSSION OF TECHNICAL CONSIDERATIONS

In the design of buildings, architects are sometimes asked to incorporate large amounts of windows into the 25 building design to increase the feeling of openness and light and/or to achieve a particular exterior aesthetic. However, windows are a major source of energy transfer either into or out of a building's interior. Energy transfer across a window glazing comprises: (1) heat flow into or out of a building due 30 to a difference between indoor and outdoor temperatures, and (2) energy transfer into a building due to solar energy transmitted and/or absorbed by the window glazing. The type of glazing that is optimal for any climate depends upon what energy transfer mechanisms have the most impact on the heating and/or cooling costs of the building and the respective

lengths of the cooling and heating seasons in that geographic location.

Energy transfer due to the indoor-outdoor temperature difference is further subdivided into three 5 different transport mechanisms: (a) conduction through the glazing and its gas contents, (b) convection associated with the movement of gases (e.g. air) at all surfaces of the glazing, and (c) thermal radiation from the surfaces of the various glazing materials. In order to reduce energy transfer 10 across window glazings, multi-pane insulating glass (IG) units have been developed. Such multi-pane IG units inhibit energy transfer via conduction and convection pathways by creating an insulating gas pocket. However, the instant invention is most germane to energy transfer caused by thermal radiation and 15 direct solar heat gain. Hereinafter, we therefore direct our discussion of energy transfer mostly to thermal radiation and direct solar heat gain rather than that due to conduction or convection. Of course the latter two energy transfer pathways should always be considered in building glazing design.

Considering thermal radiation and direct 20 solar heat gain, mainly in warm climates, energy enters into the building through the window glazing via several energy mechanisms. These include: (1) long-wave thermal infrared (IR) energy (i.e. heat) radiated from hot exterior surfaces such as pavement and buildings, and (2) the shorter wavelength ultraviolet, visible, and near infrared (or "solar infrared") radiation from the sun. The first is due to the fact that the outdoor temperature is higher than the indoor temperature. The second is either directly transmitted through the window 30 or is first absorbed by the window glazing materials and then partially re-radiated into the interior space of the building. It is relevant to note that nearly all of the incident solar energy at the earth's surface falls almost approximately equally within the visible and solar infrared portions of the spectrum with a much smaller portion falling in the

ultraviolet. The heat load contribution from the solar ultraviolet is much less than the amount of energy in the visible and solar infrared.

In cold climates, interior heat is lost through the
windows thereby increasing the energy costs required to
maintain a desired interior temperature. This loss is because
the indoor temperature is higher than the outdoor temperature.
In the case of cold climates, the heat loss due to the indooroutdoor temperature difference is partially offset by the
desirable passive solar heating of the interior space during
daylight hours.

Radiative energy loss from a surface is governed by the surface's emissivity. Emissivity relates to the propensity of the surface to radiate energy. For surfaces

15 near room temperature, this radiated energy falls within the long-wavelength thermal infrared portion of the electromagnetic spectrum. High-emissivity surfaces are good thermal radiators; a blackbody is a perfect radiator and is defined as having an emissivity of unity (e = 1). In

20 comparison, uncoated clear float glass has an emissivity of about 0.84, which is only around 16 percent less than a black body.

Radiative energy transfer across a window glazing can be inhibited by reducing the emissivity of one or more surfaces of the glass. This emissivity reduction can be realized by the use of so-called "low emissivity" or "low-E" coatings applied to the glass surface(s). Low emissivity coated glasses are attractive for architectural windows since they significantly reduce the costs of heating a building in cold climates. These low-E coatings typically comprise multilayer thin film optical stacks. The optical stacks are designed to have high reflectance in the long-wavelength thermal infrared thereby inhibiting heat transfer due to radiation across the glazing whilst retaining a high level of luminous transmittance and low luminous reflectance in the

shorter-wavelength visible portion of the spectrum. In this manner the coated glass does not dramatically depart from the visual appearance of an uncoated pane of glass. Such coatings are typically referred to as "high-T/low-E" coatings. Over 5 the past twenty years, the use of such spectrally-selective high-T/low-E coated glasses has achieved widespread marketplace acceptance in cool climates. In these climates the heating seasons are long and the passive solar heating achieved through the use of such high luminous transmittance 10 coatings assists in counteracting heat loss due to indooroutdoor temperature differences. One main type of such high-T/low-E coatings comprise one or more infrared-reflective layers (typically noble metals such as silver) sandwiched between dielectric layers (typically metal oxides or certain 15 metal nitrides). Examples of low emissivity coatings are found, for example, in United States Patent Nos. 5,821,001; 5,028,759; 5,059,295; 4,948,677; 4,898,789; 4,898,790; and 4,806,220, which are herein incorporated by reference.

However, because conventional high-T/low-E windows 20 generally transmit a relatively high percentage of visible light, and solar infrared ("near infrared") radiation to a somewhat lesser degree, use of such coatings can result in increased heat load to a building's interior in the summer season, thus increasing cooling costs. Although this problem is important for all types of buildings (such as residential 25 homes) in warm climates, it is particularly acute for socalled "commercial" architecture; that is, buildings that house office space or other facilities primarily intended for the purposes of business and commerce like office towers, 30 business parks, high-rise hotels, hospitals, stadiums, and tourist attractions. Conventional high-T/low-E coated glasses do impart some degree of heat load reduction in hot climates because the low-E coating reduces the thermal infrared load from hot exterior surfaces into the building's interior.

35 However they do not shade the building's interior as

effectively from directly transmitted and absorbed solar energy.

As a point of terminology, the ability of a window glazing to shade the interior space from transmitted and 5 absorbed solar energy is characterized by a parameter known as the glazing's "shading coefficient" (hereinafter referred to as "SC"). The term "shading coefficient" is an accepted term in the field of architecture. It relates the heat gain obtained when an environment is exposed to solar radiation 10 through a given area of opening or glazing to the heat gain obtained through the same area of 1/8 inch (3 mm) thick single-pane clear uncoated soda lime silicate glass under the same design conditions (ASHRAE Standard Calculation Method). The 1/8 inch thick clear glass glazing is assigned a shading 15 coefficient of SC = 1.00. A shading coefficient value below 1.00 indicates better heat rejection than single-pane clear glass. A value above 1.00 would be worse than the baseline clear single pane glazing.

Conventional silver-based high-T/low-E coated

20 glasses, briefly described above, typically have SCs of about
 0.44 to about 0.70 and luminous (visible) light transmittance
 of about 71% to about 75%. All of these values are referenced
 to a double-glazed IG unit installation having clear glass
 substrates. With such SCs, conventional high-T/low-E coated

25 glasses are less optimal for hot climates.

What is needed and desirable, for at least hot climates as an object of the present invention are coatings to give transparency articles like window glazings (1) low-emissivity to inhibit heat ingress from the hot exterior via thermal radiation and, (2) low transmittance and/or low absorbance of direct solar radiation through the glazing. This should be accomplished while maintaining acceptable visible light transmission through the glazing.

SUMMARY OF THE INVENTION

The present invention is directed to a low emissivity, low shading coefficient, low reflectance multilayer coating and coated article. The coating provides a 5 coated article of a transparent or at least translucent substrate with a surface comprising the coating of: at least one antireflective layer deposited over a substrate surface; and at least one infrared reflective layer deposited over the at least one antireflective layer, such that the coated 10 article comprises a visible light transmittance of greater than about 50%, a shading coefficient of less than about 0.33 and a luminous exterior and/or interior reflectance of less than about 30%. The coated article, e.g. an IG unit, also preferably has a substantially neutral color in reflectance 15 and a blue or blue-gray color in transmission. The latter value is based or measured for a double-glazed IG unit employing clear glass substrates.

The multi-layer coating of the present invention is a middle-T/low-SC/low-E coating as opposed to a high-T/low-E 20 type coating for transparencies. The "T" refers to luminous (visible) light transmittance and the "E" refers to emissivity. The middle-T is generally in the range of greater than about 50% and suitably about 50% to about 70%. coating is comprised of several primary layers that may be 25 comprised of one or more films. These primary layers can be a first antireflective layer, a first infrared reflective layer, a first primer layer, second antireflective layer, second infrared reflective layer, second primer layer, and a third antireflective layer. Optionally the one or more protective These layers are arranged 30 overcoats can be present. predominantly in the order stated one on top of the other over a substantial portion if not all of one or more surfaces of the substrate. Any portion of the surface of the substrate can be coated. Suitably when at least one surface of the substrate that is exposed to light is coated, increased

benefits from the invention are realized. The aforementioned layers of the inventive coating are primary layers in that other films or layers can be between the layers themselves or the stacks of the layers as long as these secondary layers or films do not interfere with the functioning of the primary layers.

The thickness of the layers of the coating is such that the individual infrared reflective layers are not increased to be greater than that for high-T/low-E coatings. 10 Increasing the thickness of the infrared reflective layer like silver layer(s) much beyond that for high T/low E coatings both increases the long-wavelength thermal infrared reflectivity and increases the shorter-wavelength solar infrared reflectivity. Even though the latter lowers the 15 shading coefficient, the former reduces emissivity. Also in regards to the spectral characteristics of the infrared reflective layers, like silver thin films, simply increasing the thickness of the silver layer or film will simultaneously tend to increase the coating's reflectance and decrease the coating's transmittance in the visible region of the electromagnetic spectrum. This is an important aesthetic issue concerning the variation of reflected and transmitted colors of the coated article with the angle of observation. Such thicker silver layer(s) will tend to produce coatings 25 that acquire reflected colors having unacceptable red or pink or orange components viewed either at normal incidence or at an oblique (grazing) angle.

Also in the present invention the thickness of the individual antireflective layers adjacent to the infrared

reflective layers are not offset to some extent to compensate for any increased visible reflectance and decreased visible transmittance from any such increased thickness of the infrared reflective layers. Such modification of the physical (and therefore optical) thickness of the adjacent dielectric layers (antireflective layer) to anti-reflect the silver

layer(s) in the visible and to adjust the transmitted and
reflected color of the coated article is possible. Although
an improvement may be viewed at normal incidence, the
reflected color viewed at oblique incidence may remain
objectionable, or vice versa. However, the optical
characteristics of real thin film dielectric materials impose
constraints on the efficacy of such an anti-reflection
approach.

The coated article of the present invention is a 10 transparent or translucent substrate usually with two major surfaces as in the form of a flat, contoured, or curved sheet with the aforementioned coating on at least one of the surfaces. Also an embodiment of the present invention is an insulated glass unit (hereinafter referred to as "IG-unit"). 15 In the IG-unit at least two transparent substrates are sealed together with a space or gap between them generally for transparent insulating materials usually of a gaseous nature. The IG-unit can have any surface of the substrate with the aforementioned coating but suitable surfaces are either or 20 both of the interior surfaces of the IG-unit. Also the coating could be arranged on one or more polymeric films or foils that is placed in the gap in the IG-unit. When the coating is disposed on the surface of the transparent substrate in an IG-unit the coating can be on at least one of 25 the surfaces but preferably is on one of the surfaces facing the gap. The substrates in the IG-unit can be clear or tined or colored transparent or translucent glass or plastic. For instance the coating can be on one of the interior surfaces of a substrate in the IG-unit which is clear or colored or tinted and the other substrate without the coating can be tinted or colored glass or plastic rather than clear or untinted or uncolored.

The present invention accounts for the interdependence of solar performance, emissivity, and normal/oblique aesthetics, and in view of the limitations of

real thin film optical materials, meets the challenge of producing a low-emissivity, solar-control coating having acceptable aesthetics. Such an article with such a coating can maintain acceptable aesthetics for transparencies for 5 architectural, automotive, aerospace, or other such applications.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a cross-sectional view, not to scale, of a 10 coating incorporating features of the invention; and Fig. 2 is a cross-sectional view of an IG unit incorporating features of the invention.

DESCRIPTION OF THE INVENTION

For purposes of the following discussion, the phrase "deposited over" means deposited above but not necessarily adjacent to. Additionally, directional terms such as "left", "right", "inner", "outer", "upper", "lower", etc., and similar terms shall relate to the invention as it is shown in the 20 drawing figures. However, it is to be understood that the invention may assume various alternative orientations. Hence, such terms are not to be considered as limiting. Also, the terms "coating" or "coating stack" include one or more coating layers and/or coating films. The terms "coating layer" or "layer" include one or more coating films. Also patents and published patent documents listed in this disclosure are hereby incorporated by reference in total and specifically for that which the patents are noted as teaching. Additionally in the following discussion the numerical ranges or values for 30 the percentage of materials and for the thickness of all of the individual layers and films and coatings are approximate and may vary slightly below the lower limit and above the upper limit or around the specifically stated number as though preceded by the word "about" for each.

A substrate 10 having a low emissivity, low shading coefficient coating 12 incorporating features of the invention is generally shown in Fig. 1. The substrate 10 may be of any material but in the practice of the invention is preferably a 5 transparent substrate, such as glass, plastic or ceramic. However, tinted or colored substrates may also be used. In the following discussion, the substrate 10 is preferably glass. Examples of glass suitable for the practice of the invention are described, for example, in United States Patent 10 Nos. 4,746,347; 4,792,536; 5,240,886; 5,385,872; and 5,393,593.

The coating 12 is a multilayer coating and is deposited over at least a portion of the substrate surface in conventional manner. For example, the coating 12 may be 15 applied by magnetic sputter vapor deposition (MSVD), chemical vapor deposition (CVD), spray pyrolysis, sol-gel, etc. In the currently preferred practice of the invention, the coating 12 is applied by MSVD. MSVD coating techniques are well known to one of ordinary skill in the glass coating art and hence will 20 not be discussed in detail. Examples of MSVD coating methods are found, for example but not to be considered as limiting, in U.S. Patent Nos. 5,028,759; 4,898,789; 4,948,677; 4,834,857; 4,898,790; and 4,806,220.

The coating 12 includes a base layer or first antireflective layer 14 deposited over at least a portion of 25 one of the substrate surfaces. The first antireflective layer 14 preferably comprises one or more films of dielectric materials or antireflective materials such as metal oxides or oxides of metal alloys which are preferably transparent or substantially transparent. Examples of suitable metal oxides include oxides of titanium, hafnium, zirconium, niobium, zinc, bismuth, lead, indium and tin and mixtures of any or all of these. These metal oxides may have small amounts of other materials, such as manganese in bismuth oxide, indium in tin 35 oxide, etc. Additionally, oxides of metal alloys, such as

zinc stannate or oxides of indium-tin alloys can be used. Further, doped metal oxides, such as antimony-, fluorine- or indium-doped tin oxides or mixture thereof can be used. the practice of the invention, the first antireflective layer 5 14 preferably comprises one or more oxides of zinc and tin. The first antireflective layer 14 may be a substantially single phase film such as zinc stannate or may be a mixture of phases composed of zinc and tin oxides or may be composed of a plurality of metal oxide films, such as those disclosed in 10 U.S. Patent No. 5,821,001. Preferably, the first antireflective layer 14 comprises one or more oxides of zinc and tin, e.g. zinc stannate. The first antireflective layer 14 preferably has a thickness in the range of 272 to 332 Angstroms, more preferably around 293 Angstroms. In a 15 currently preferred embodiment of the invention, the first antireflective layer 14 is a multifilm structure as disclosed in U.S. Patent No. 5,821,001 having a zinc stannate film deposited over the substrate surface and a zinc oxide film deposited over the zinc stannate film. The zinc stannate film is sputtered using a zinc-tin cathode which is 52 wt% zinc and 20 48 wt% tin. The zinc oxide film is deposited from a zinc cathode having 10 wt% or less of tin. The zinc oxide film has

antireflective layer 14 a single zinc stannate film.

A first IR reflective layer 16 is deposited over the first antireflective layer 14. The first IR reflective layer 16 is preferably an IR reflective metal, such as gold, platinum, copper, silver, or alloys or mixtures of any or all of these that are IR reflective. In the preferred embodiment of the invention, the first IR reflective layer 16 comprises silver and preferably has a thickness in the range of 80 to 269 Angstroms, more preferably 86 Angstroms.

a preferred thickness of 20 to 70 Angstroms in the layer as disclosed in U.S. Patent No. 5,821,001. It is also possible that the zinc oxide film may be less than this thickness or

may be omitted entirely thereby rendering the first

A first primer layer 18 which is preferably at least one film is deposited over the first IR reflective layer 16. The first primer layer 18 is a material and deposited at such a thickness to minimize exposure of the silver layer to 5 reaction from a subsequently applied reactive plasma for film or layer deposition. Preferably the primer layer is at least one oxygen capturing film, such as titanium, that is sacrificial during the deposition process to prevent degradation of the first IR reflective layer 16 during the 10 sputtering process. The first primer layer 18 preferably has a thickness of 8 to 30 Angstroms, most preferably 8 to 20 Angstroms as disclosed in U.S. Patent No. 5,821,001. For tempering of glass, the thickness of the primer layer can be increased and the thickness of the other layers can be altered 15 to match or exceed the aesthetics and/or performance of the untempered glass.

A second antireflective layer 20 is deposited over the first primer film 18. The second antireflective layer 20 preferably comprises one or more metal oxide or metal alloy oxide films, such as those described above with respect to the first antireflective layer 14. In the currently preferred practice of the invention, the second antireflective layer 20 has a first film of zinc oxide deposited over the first primer film 18. A zinc stannate film is deposited over the first zinc oxide film and a second zinc oxide film is deposited over the zinc stannate film to form a multi-film antireflective layer. Each zinc oxide film of the second antireflective layer 20 is preferably 20 to 70 Angstroms thick, although the zinc oxide film may be less than this thickness. The second antireflective layer 20 preferably has a total thickness of 698 to 863 Angstroms, more preferably 719 Angstroms.

A second IR reflective layer 22 is deposited over the second antireflective layer 20. The second IR reflective layer 22 is preferably silver and most preferably a silver film although any of the materials listed for the first IR reflective layer 16 and has a thickness of 159-257 Angstroms, more preferably 170 to 180 Angstroms.

A second primer layer 24 is deposited over the second IR reflective layer 22. The second primer layer 24 is preferably titanium having a thickness of 8-20 Angstroms.

A third antireflective layer 26 is deposited over the second primer layer 24. The third antireflective layer 26 is also preferably one or more metal oxide or metal alloy oxide containing films such as discussed above with respect to the first antireflective layer 14. In practice, the third antireflective layer 26 includes a zinc oxide film of 20 to 70 Angstroms deposited over the second primer layer 24 as disclosed in U.S. Patent No. 5,821,001. However the zinc oxide film may be less than this thickness or may be omitted entirely and a zinc stannate film can be deposited over this zinc oxide film. The third antireflective layer 26 has a total thickness of 60-273 Angstroms, preferably 115 Angstroms.

A protective overcoat 28 is deposited over the third antireflective layer 26 to provide protection against mechanical and chemical attack. The protective overcoat 28 is 20 preferably an oxide of titanium like titanium dioxide having a thickness of 30-45 Angstroms. Alternatively or in addition thereto, a protective coating, such as one or more oxides or oxynitrides of silicon or one or more oxides of aluminum or 25 mixtures or combinations of any of these, may be deposited over the titanium dioxide coating or in lieu thereof. Examples of suitable protective coatings are disclosed, for example, in U.S. Patent Application No. 09/058,440 and in U.S. Patent Nos. 4,716,086; 4,786,563; 4,861,669; 4,938,857; and 30 4,920,006 and Canadian Application No. CA 2,156,571. In lieu of or in addition to the protective overcoat 28, temporary or removable protective films, layers or coatings can be used such as solvent soluble organic coatings like those describe in U.S. Patent Application Serial Number 09/567934, filed 10-35 May-2000, and similar to PCT application number WO US00/17326

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outwardly facing or outer surface 54 and an inwardly facing or inner surface 56. The multi-layer coating 12 of the invention is preferably deposited either on the inner surface 52 of the exterior glass piece 42, as shown in Fig. 2, or the outer surface 54 of the interior glass piece 44. As discussed hereinbelow, the IG unit 40 having the coating 12 of the invention provides a visible light transmittance of greater than about 50%, preferably 55%; a shading coefficient of less than about 0.33; and an exterior reflectance of less than about 30% when normally positioned, e.g. the outer surfaces directed to the exterior of the structure and the inner surfaces directed to the interior of the structure.

EXAMPLES

Coatings were prepared in accordance with the invention and analyzed for optical qualities. The coating layers were deposited at the specified thickness as shown in Table I on pieces of clear float glass of the thickness shown in Table I by MSVD for an IG unit. In the IG unit the coated glass was as reference number 44 and the coating as reference number 54 in Fig, 2. The structure of the coated samples is given in Table I, with the layer thickness given in Angstroms. In each sample, the first, second and third antireflective layers (AR layers) were multifilm zinc oxide and zinc stannate structures as described above. The numbers in Table I are for the total thickness of the specific layers, with each individual zinc oxide film in an AR layer being about 50 to 60 Angstroms thick. The first and second IR reflective layers (IR layers) were silver and the primer layers were titanium. The overcoat was titanium dioxide. The notation ND means that no data was taken.

	Table I										
	Glass										
	thick-										
Sample	ness	1 st						3 rd	Over-		
No.	inch	AR	Ag	Ti	2 nd AR	2 nd Ag	Ti	AR	coat		
1	0.1596	332	128	15	771	246	15	168	45		
2	0.0862	312	236	15	698	159	15	202	45		
3	0.0863	272	236	15	845	192	15	196	45		
4	0.0863	313	246	15	863	210	15	250	45		
5	0.126	300	86	13	714	175	13	123	30		
6	0.126	300	86	13	714	175	13	60	30		
7	0.125	300	95	13	734	184	13	98	30		
8	0.126	300	103	13	808	202	13	194	30		
9	0.126	300	107	13	734	167	13	98	30		
10	0.126	300	103	13	714	184	13	98	30		
11	0.124	293	80	17	719	178	15.5	105	43		
12	0.123	293	86	17	695	178	15.5	105	43		
13	0.125	293	86	17	719	178	15.5	115	43		

The optical and performance characteristics of the samples of Table I are shown in Table II. The optical characteristics in Table II are calculated values ("center of glass") for either a monolithic piece of glass or an IG unit incorporating the respective sample coatings. These calculations used the spectrophotometric data and the "WINDOW" 4.1 simulation software program available from Lawrence Berkeley National

Laboratory. All of the optical characteristics in Table II, with the exception of LCS, are standard and well known terms in the glass industry. The term "LCS" refers to a light to cooling selectivity index and is defined as the percent visible light transmittance (expressed as a decimal) divided by the shading coefficient.

				e e	CT'	0	0	0	σ	o	0	o	6	0	6	0	0
			Winter	U-value	0.24	0.29	0.30	0:30	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.30	0.30
				Emissivity	0.03	0.029	0.041	0.039	0.032	0.032	0.033	0.029	0.031	0.029	0.029	0.048	0.048
				LHS	2.21	2.27	2.29	2.36	2.03	2.05	2.04	2.08	2.09	2.13	2.01	2.04	2.00
				rcs	1.90	1.96	1.97	2.03	1.72	1.71	1.77	1.80	1.83	1.83	1.70	1.77	1.75
HI		Solar heat	gain	coefficient	0.25	0.25	0.25	0.25	0.28	0.25	0.26	0.26	0.28	0.25	0.27	0.27	0.28
Table		Summer	shading	coefficient	0.29	0.29	0.29	0.29	0.33	0.30	0.30	0.30	0.32	0.29	0.32	0.31	0.32
		% int vis	reflect-	ance	29.2	20.4	24.5	22.3	29.1	35.5	33	31.8	26.6	31.6	32.5	31.4	30.6
	% ext	vis	reflect-	ance	21.8	25.3	25.7	23.8	21.9	26.3	24.7	25.5	19.8	22.2	25.1	23.4	23.5
				% VIS	55.2	56.8	57.2	58.9	56.7	51.2	53.1	54.1	58.6	53.2	54.3	55.0	56.0
			Sample	No.	П	2	т	4	Ω.	9	7	8	6	10	11	12	13

 $\begin{tabular}{ll} Table III shows several listed physical parameters \\ for monolithic glass samples coated with coating of Table I \\ and listed performance data for these glasses. \\ \end{tabular}$

				-		coated	surface	emissivity	0.030	0.029	0.041	0.039	0.032	0.032	0.033	0.029	0.031	0.029	0.029	0.048	0.048
							S	THS		2.07	2.08	2.14	1.99	1.98	2.06	2.03	2.06	2.14	1.96	1.99	1.96
								rcs		1.77	1.78	1.89	1.72	1.73	1.75	1.78	1.78	1.81	1.68	1.71	1.74
	center-of-glass)	solar heat	gain	coefficient	(energy	incident on	coated	surface)		0.30	0.30	0.30	0.31	0.28	0.28	0.29	0.31	0.27	0.30	0.30	0.31
	are center-c	summer	shading	coefficient	(energy	incident on	coated	surface)	0.38	0.35	0.35	0.34	0.36	0.32	0.33	0.33	0.36	0.32	0.35	0.35	0.35
III	data					TSER-	coating-	Side (%)	60.7	59.2	60.2	60.7	61.5	65.4	65.0	61.1	61.6	65.8	62.8	63.2	62.3
Table I	Data (all				TSER-	glass-	sıde	(%)	37.9	51.3	51.3	51.7	40.0	42.3	42.7	42.4	40.6	43.4	40.9	41.4	40.9
	1						TSET	(%)	28.2	25.3	25.1	24.8	27.5	24.6	24.7	25.1	27.1	23.8	26.8	26.4	27.2
	ic Performance			coating-	side	visible	reflectance	(%)	25.3	14.2	18.9	16.4	25.0	32.5	29.6	28.1	21.9	27.9	29.0	27.7	26.8
	Monolithi				glass-side	visible	reflectance	(8)	18.6	21.9	22.3	20.2	18.6	23.5	21.8	22.5	16.2	19.2	22.0	20.3	20.3
					visible	trans-	mittance	(%)	60.3	62.1	62.3	64.2	61.8	55.4	57.6	58.8	64.0	57.8	58.9	59.7	6.09
				clear	glass	thick-	ness	(inch)	0.1596	0.0862	0.0863	0.0863	0.126	0.126	0.125	0.126	0.126	0.126	0.124	0.123	0.125
							Sample	ID	П	2	3	4	5	9	7	00	6	10	11	12	13

The results of mechanical and chemical durability tests conducted on the samples are shown in Table IV.

	Table IV								
Sample	Initial	Salt	Ammonium	Acetic	DART	ccc	Taber		
No.	Haze	Test	Test	Acid	210		Test		
1	ND	ND	ND	ND	ND	ND	ND		
2	ND	ND	ND	ND	ND	ND	ND		
3	ND	ND	ND	ND	ND	ND	ND		
4	ND	ND	ND	ND	ND	ND	ND		
5	12.0	9.0	10.0	9.0	9.5	8.5	65		
6	11.0	8.5	9.0	8.5	9.0	7.0	ND		
7	11.0	9.0	9.5	9.5	9.0	9.0	62		
8	11.0	9.0	9.0	9.5	9.0	8.5	ND		
9	11.0	9.0	9.0	9.5	8.5	9.0	63		
10	11.0	8.5	9.0	8.0	8.5	6.0	ND		
11	9.0	9.0	9.0	9.5	9.0	9.0	58		
12	9.5	9.0	9.0	9.0	9.5	9.0	56		
13	9.3	9.0	9.3	9.5	9.0	9.3	63		

The haze ratings shown in Table IV are based on a twelve unit system, with twelve being substantially haze free and lower numbers indicating increasing levels of haze. In the following discussion unless indicated to the contrary, the observation for haze was performed as follows. A coated piece of glass ("coupon") was treated in accordance with the particular test being conducted. The coupons were individually observed with the unaided eye in a dark room with about 150 watt flood light. The coupon was placed in front of the light, and its position was adjusted relative to the light to maximize haze. The observed haze was then rated.

The salt water test consists of placing the coated glass pieces or coupons in a 2.5 weight percent (wt%) solution of sodium chloride in deionized water for 2.5 hours. The

coupons were removed, rinsed in deionized water and dried with pressurized nitrogen and then rated for haze.

In the ammonium hydroxide test a test coupon was placed in a 1 Normal solution of ammonium hydroxide in deionized water at room temperature for 10 minutes. The coupon was removed from the solution, rinsed in deionized water and dried as discussed above. The test coupon was examined for haze.

In the acetic acid test a test coupon was submerged in a 1 normal solution of acetic acid in deionized water at room temperature for 10 minutes. The test coupon was removed from the solution and rinsed off with deionized water and blown dry using high pressure nitrogen. The test coupon was examined for haze.

The Cleveland Condensation Chamber (CCC) test is a well-known test and is not discussed in detail herein. The test coupons were exposed to the CCC test for a period of time with warm water vapor and examined for haze. The abbreviation "ND" stands for "no data".

20 The Taber test is also a well known test and will not be described in detail. Generally the modified Taber test comprises securing the sample to be tested on a flat, circular turntable. Two circular, rotating Calibrase® CS-10F abrasive wheels (commercially available from Taber Industries of N.

Tonawanda, NY) are lowered onto the top surface of the sample

to be tested; there is a load of 500 grams applied to each abrasive wheel. The Calibrase® CS-10F wheels are an elastomeric-type material that is impregnated with an abrasive. To conduct the test, the turntable is switched "ON" and the abrasive wheels turn and abrade the sample's surface as the sample and turntable rotate about a vertical axis until the desired number of rotations or "cycles", here 10, is completed. After testing, the sample is removed from the turntable and examined for damage to the top surface. The numbers in Table IV denote the scratch density per square

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millimeter for a black and white micrograph at a 50X magnification.

Thus, the present invention provides a low emissivity, solar control article, e.g. an IG unit, having 5 visible light transmission of greater than about 50%, a shading coefficient less than about 0.33 and an exterior reflectance less than about 30%. Such an article is particularly well adapted for use in warmer climates to help reduce cooling costs for the interior of a structure.

In a preferred embodiment, a solar control coated article of the invention comprises a substrate with a first antireflective layer deposited over at least a portion of the substrate. A first infrared reflective film is deposited over the first antireflective layer and a first primer film is 15 deposited over the first infrared reflective film. A second antireflective layer is deposited over the first primer film and a second infrared reflective film is deposited over the second antireflective layer. A second primer film is deposited over the second infrared reflective film and a third antireflective layer is deposited over the second primer film, such that the coated article has a transmittance greater than about 55%, a shading coefficient of less than about 0.33 and a reflectance of less than about 30%. A protective overcoat, e.g. an oxide or oxynitride of titanium or silicon, may be 25 deposited over the third antireflective film.

It will be readily appreciated by those skilled in the art that modifications may be made to the invention without departing from the concepts disclosed in the foregoing description. Such modifications are to be considered as included within the scope of the invention. Accordingly, the particular embodiments described in detail hereinabove are illustrative only and are not limiting as to the scope of the invention, which is to be given the full breadth of the above disclosure and any and all equivalents thereof.

What is claimed is:

- 1. A solar control article, comprising:
- a substrate having a surface;
- at least one antireflective layer deposited over the 5 substrate surface; and
 - at least one infrared reflective film deposited over the at least one antireflective layer,

such that the coated article has a transmittance greater than about 55%, a shading coefficient less than about 0.33 and a reflectance less than about 30%.

- The article as claimed in claim 1, wherein the article includes a first antireflective layer, a second antireflective layer, a third antireflective layer, a first 15 infrared reflective layer and a second infrared reflective layer, with the first infrared reflective layer deposited over the first antireflective layer and the second infrared reflective layer deposited over the second antireflective layer and with the third antireflective layer deposited over the second infrared reflective layer.
- The article as claimed in claim 2, including a first primer layer deposited over the first infrared reflective layer and a second primer layer deposited over the 25 second infrared reflective layer.
- The article as claimed in claim 2, wherein the antireflective layers include metal-oxide films selected from one or more metal oxides, oxides of metal alloys, doped metal 30 oxides and mixtures thereof.
- 5. The article as claimed in claim 2, wherein the one or more metal oxides are selected from zinc oxide, titanium oxide, hafnium oxide, zirconium oxide, niobium oxide, 35 bismuth oxide, indium oxide, tin oxide and mixtures thereof.

- 6. The article as claimed in claim 2, wherein the metal alloys are selected from the group consisting of zinc stannate, tin alloys, fluorine doped tin, antimony doped tin, and indium—tin alloys.
 - 7. The article as claimed in claim 2, wherein at least one of the antireflective layers comprises a plurality of antireflective films.

8. The articles as claimed in claim 2, wherein the infrared reflective films include at least one metal selected from the group consisting of gold, copper, platinum, and

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silver and mixtures thereof.

- 9. The article as claimed in claim 2, wherein the first antireflective layer has a thickness of about 272 to about 332 angstroms, the second antireflective layer has a thickness of about 198 to about 836 angstroms and the third antireflective layer has a thickness of about 60 to about 273 angstroms.
 - 10. The article as claimed in claim 2, wherein the first infrared reflective layer has a thickness of about 86 to about 269 angstroms and the second infrared reflective layer has a thickness of about 159 to about 257 angstroms.
- 11. The article as claimed in claim 3, wherein the first and second primer layers each have a thickness of about 30 15 to about 30 angstroms.
- 12. The article as claimed in claim 2, wherein the thickness of the second infrared reflective layer is about 50 to about 100% greater than the thickness of the first infrared reflective layer.

13. The article as claimed in claim 2, including a protective overcoat deposited over the third antireflective layer.

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- 14. The article as claimed in claim 1, wherein the substrate is selected from the group consisting of glass, plastic and ceramic.
- 10 15. The article as claimed in claim 1, wherein the article is an insulated glass unit.
 - 16. A solar control coated article, comprising:
 a substrate having a surface;
- a first antireflective layer deposited over a substrate surface;
 - a first infrared reflective layer deposited over the first antireflective layer;
 - a first primer layer deposited over the first infrared reflective layer;
 - a second antireflective layer deposited over the first primer layer;
 - a second infrared reflective layer deposited over the second antireflective layer;
 - a second primer film deposited over the second infrared reflective layer; and
 - a third antireflective layer deposited over the second primer layer, such that the coated article has a transmission of greater than about 55%, a shading coefficient of less than about 0.33 and an external reflectance of less than about 30%.
 - 17. The article as claimed in claim 16, wherein the article has a substantially neutral color.

18. The article as claimed in claim 16, wherein the article has a transmittance greater than about 55%, a shading coefficient of less than about 0.32 and an external reflectance less than about 20%.

19. The article as claimed in claim 16, wherein the substrate is selected from the group consisting of glass, plastic and ceramic.

- 20. The article as claimed in claim 16, wherein the antireflective films include a metal oxide film selected from the group consisting of metal oxides, metal alloys, doped metal oxides and mixtures thereof.
- 15 21. The article as claimed in claim 20, wherein in the metal oxides are selected from the group consisting of zinc oxide, titanium oxide, hafnium oxide, zirconium oxide, niobium oxide, bismuth oxide, indium oxide, tin oxide and mixtures thereof.

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22. The article as claimed in claim 20, wherein the metal alloys are selected from the group consisting of zinc stannate, fluorine doped tin, antimony doped tin, and indiumtin alloys.

- 23. The article as claimed in claim 20, wherein the doped metal oxides are selected from the group consisting of antimony doped tin oxide and indium doped tin oxide.
- 24. The article as claimed in claim 16, wherein the first infrared reflective layer includes a metal from the group consisting of gold, copper, platinum, and silver and mixtures thereof.

- 25. The article as claimed in claim 16, where at least one of the first, second, or third antireflective layers includes a plurality of antireflective films.
- 5 26. The article as claimed in claim 16, wherein the primer layer includes titanium.
- 27. The article as claimed in claim 16, including a protective, metal containing overcoat deposited over the third antireflective layer.
 - 28. The article as claimed in claim 16, wherein the article is an insulated glass unit.
- 15 29. The article as claimed in claim 16, wherein the first antireflective layer has a thickness of about 272 to about 332 angstroms, the second antireflective layer has a thickness of about 198 to about 836 angstroms and the third antireflective layer has a thickness of about 60 to about 273 angstroms.
- 30. The article as claimed in claim 16, wherein the first infrared reflective layer has a thickness of about 86 to about 269 angstroms and the second infrared reflective layer has a thickness of about 159 to about 257 angstroms.
 - 31. The article as claimed in claim 16, wherein the first and second primer layers each have a thickness of about 15 to about 30 angstroms.

32. A method of making a solar control article, comprising the steps of:

providing a substrate having a surface; depositing at least one antireflective layer over the substrate surface; and

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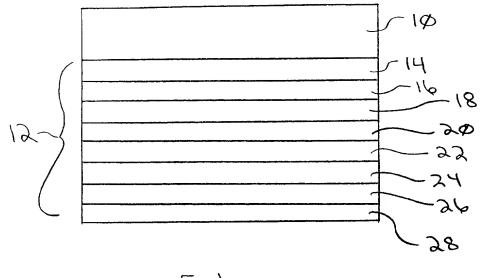
depositing at least one infrared reflective layer over the at least one antireflective layer such that the coated article has a transmittance greater than about 55%, a shading coefficient less than about 0.33 and a reflectance less than about 30%.

- 33. The method as claimed in claim 32, including depositing a first infrared reflective film over a first antireflective layer, depositing a second infrared reflective film over a second antireflective layer and depositing a third antireflective layer over the second infrared reflective film.
- 34. The method as claimed in claim 32, including 15 depositing a first primer film over the first infrared reflective film and depositing a second primer film over the second infrared reflective film.
- 35. The method as claimed in claim 32, wherein the 20 article has a substantially neutral color.
- 36. The article as claimed in claim 32, wherein the antireflective layer depositing step is practiced by depositing a plurality of antireflective films to form the at least one antireflective layer.
 - 37. The method as claimed in claim 33, wherein the first infrared reflective film has a thickness of about 86 to about 269 angstroms and the second infrared reflective film has a thickness of about 159 to about 257 angstroms.
 - 38. The method as claimed in claim 34, wherein the first and second primer films each have a thickness of about 15 to about 20 angstroms.

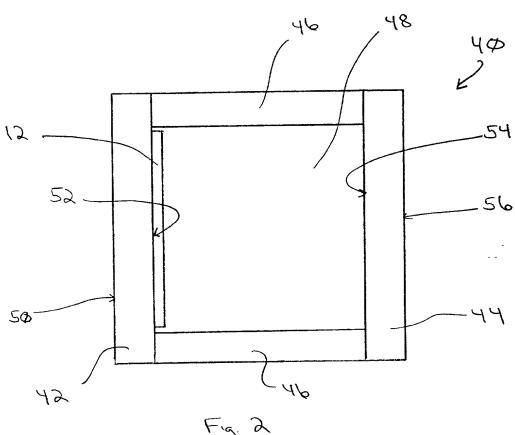
ABSTRACT OF THE DISCLOSURE

The present invention is directed to a low emissivity, low shading coefficient, low reflectance multilayer coating and coated article having a visible light 5 transmittance of greater than about 50%, preferably greater than about 55%, a shading coefficient of less than about 0.33 and en exterior reflectance of less than about 30%. coated article, e.g. an IG unit, has a substrate with a first antireflective layer deposited over the substrate. 10 infrared reflective layer is deposited over the first antireflective layer and a first primer layer is deposited over the first infrared reflective layer. A second antireflective layer is deposited over the first primer layer and a second infrared reflective layer is deposited over the 15 second antireflective layer. A second primer layer is deposited over the second infrared reflective layer and a third antireflective layer is deposited over the second primer layer, such that the coated article has a transmittance greater than about 55%, a shading coefficient of less than 20 about 0.33 and a reflectance of less than about 30%. A protective overcoat, e.g. an oxide or oxynitride of titanium or silicon, and/or solvent soluble organic film former may be

deposited over the third antireflective layer.



Fg. 1



Docke	t No
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Declaration and Power of Attorney For Patent Application English Language Declaration

As a below named inventor, I hereby declare that:

iviy residence, post o	mice address and citize	ensnip are as stated below next to m	y name,
first and joint inventowhich a patent is sou	r (if plural names are I ight on the invention ei FICIENT AND LOW EN	entor (if only one name is listed below isted below) of the subject matter what ntitled IISSIVITY COATINGS AND COATED A	nich is claimed and for
is attached hereto	D .		
was filed on		as United States Application No.	or PCT International
Application Numb	per		
and was amende	d on		
J. Comments of the comments of		(if applicable)	
		derstand the contents of the above in mendment referred to above.	dentified specification,
		United States Patent and Trademark lity as defined in Title 37, Code of	
Section 365(b) of ar any PCT International listed below and have	ny foreign application(s al application which de e also identified below or PCT International a	nder Title 35, United States Code, s) for patent or inventor's certificate signated at least one country other t, by checking the box, any foreign a pplication having a filing date before	, or Section 365(a) of han the United States, pplication for patent or
Prior Foreign Applica	ition(s)		Priority Not Claimed
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	(Application Serial No.)	(Filing Date)	
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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith. (list name and registration number)

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